

CENTRE D'ETUDE DE L'ENERGIE NUCLEAIRE

# Loss of electrical feed to the vital network of the BR2 reactor



# Safety impact and lessons learned

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# **Presentation content**

- General features of the BR2 reactor
- Safety functions overview
- "Vital" electrical grid loss
- Impact analysis
- Lessons learned and actions

# General features of the BR2 reactor







- BR2 = high performance material test reactor
  - Achievable flux levels (at mid plane in vessel)
    - Thermal flux: 7 10<sup>13</sup> n/cm<sup>2</sup>s to 10<sup>15</sup> n/cm<sup>2</sup>s
    - Fast flux (E>0.1MeV): 1 10<sup>13</sup> n/cm<sup>2</sup>s to 6 10<sup>14</sup> n/cm<sup>2</sup>s
  - Maximum rated power: 125MW cooling capacity of primary cooling system
    - Allowable heat flux in primary coolant
      - 470W/cm<sup>2</sup> for the driver fuel plates
        - » Demineralised light water
        - » Pressure to 1.2MPa, temperature 35-50°C
        - » 10m/s flow velocity on fuel plate
      - Up to 600W/cm<sup>2</sup> can be allowed in experiments
  - Compact core design with good access
    - Be + water moderated
    - Diverging core channels

## Reactor core geometry & access



# Safety functions of BR2

#### Reactivity control

- Shim/control rods and safety rods
  - Fail safe against loss of power
  - Powered by UPS
- SCRAM initiating instrumentation
  - Fail safe against loss of power
  - Powered by UPS
- Removal of residual heat
  - Possible by natural convection
  - Automatic isolation and bypass valves driven by hydraulic batteries
  - Controlled by redundant and independent I&C
- Confinement
  - Isolation of containment building by hydraulic system
  - I&C with UPS back-up

# Heat removal in accident conditions: historic tests





# Schematic of BR2 cooling loops



# Safety actions during reactor operation

#### SCRAM reactor

- Manual (2 control rooms)
- Overpower (flux)
- High/Low pressure drop over core
- High/Low pressure in primary loop (high pressure: evacuation)
- Low primary flow rate
- Motion of isolation/by-pass valves
- No external electrical feed (10kVac, 220Vac)
- No electrical feed for I&C (110VDC)
- Evacuation signal for staff

#### Reverse reactor

- Overpower (flux, thermal balance, N-16)
- Low pressure drop over reactor core
- High inlet/outlet temperature
- High temperature increase over core
- High radio-activity in primary/secondary loop
- Loss of automatic start up function of Diesel generators

# BR2 electrical feed networks

- External network (class 1)
  - Direct feed of non-safety related components (e.g. main primary pumps)
  - Normal feed of vital network 380VAC
  - Normal feed for battery units 110Vpc
  - Interruptions have no safety but operational impact
- Vital network (class 2 and 3)
  - Safety relevant components
  - Alternative feed by external network or diesel generators (no break system)
  - Not essential to safety
- Battery units & UPS (class 4)
  - Feed for safety instruments and actions
  - Multiple separated feeds available

# Vital electrical network feed loss events

- 2 events occurred during operating cycle in May 2017
  - May 12 and May 28: short electrical tension disruption
    - root cause: lightning impact on external network
  - Automatic decoupling between external network and vital network
  - Vital network is powered by inertia of flywheels
  - Frequency detection @49.5Hz trigger fails to start diesel engines
  - Power consumption level on vital network too low to trigger power detector to start diesel engines (normal network feeds main pumps)
  - Alternators are decoupled at @ 45Hz to protect vital network users against high currents
- Loss of automatic takeover of diesel generators trips reactor (reverse signal)

# Tension disruption on external feed network



# Decoupling between external network and vital network





# Impact of loss of vital network 12/05

- Reactivity control of reactor
  - No impact: instruments and I&C are fed by UPS
  - Reverse signal results in lowering of control rods
  - SCRAM (manual)
- Heat removal
  - Upon reverse, secondary flow is reduced by pilot to maintain primary pressure
  - After 1 minute, secondary flow stops due to closing of isolation valve on secondary side (fail close)
  - Primary pressure increases due to low heat removal
  - Evacuation due to high primary pressure
    - Closing of automatic isolation valves and opening of bypass valve
- Confinement function
  - Evacuation signal automatically isolates reactor building

#### Neutron flux observation



# Hydraulic conditions





# Primary pressure evolution



# Impact on operations and data acquisition

- Radiation monitoring equipment
  - Connected to vital network, most sensitive to electrical feed disruption
  - Measurement of radio-activity in primary water non-functional during isolation of primary loop inside reactor pool (ABV closed)
  - Radiation monitoring equipment triggers REVERSE action: non-fail safe architecture (> < SCRAM triggers)</li>
- Illumination
  - Machine control room: connected to vital network black out
  - Reactor building: 50% vital network, 50% normal network
  - Reactor control room: connected to UPS
- Control rooms
  - Reactor control room: minor impact, but evacuated
  - Machine control room
    - Synoptic panel black-out
    - Alarms & recorders powered by UPS
- DAQ: computer recording and visualization of data lost (partially)
  - No safety function

# **Recovery actions**

- Verification of safe condition of auxiliary systems/buildings: check by fire brigade
- Coupling of vital and normal network
  - First attempt unsuccessful: short restart of secondary flow and pressure drop in primary system
  - Restart of illumination and signalization on synoptic panel in machine control room
- Manual restart of radiation monitoring devices, check of absence of contamination/increased radiation levels
- Coupling of diesel unit to vital network in stand-by mode (21h00)
- Start of shut-down pumps and opening of isolation valves to verify absence of fission products in primary water (22h30)
- Restart ventilation (23h25)
- Shut-down and cool-down according to standard procedures

# Lessons learned & actions

- Black out of "vital" electrical feed is no initiating event for safety issue
  - Basic safety functions remain intact due to passive nature & redundant feeds
  - Sufficient layers of defense-in-depth
  - Basic INES evaluation = 0; +1 due to common cause loss of external feed and internal feed by diesel generators
- Failure of diesel generator start was due to 2 causes
  - Ageing issues with detection and switching devices to couple diesel generators to alternators
  - Threshold of power consumption higher than actual level during operation with external network feed available
- Test procedure and maintenance schedule revised
  - System functional test unable to identify hidden failures in parallel systems
  - Lab maintenance and test procedures for individual components
- System upgrades
  - Installation of additional switches
  - Replacement of aged components
  - Adjustment of power threshold and systematic verification of power consumption on vital network

# **Testing issues**

- Initial field test method: simulation of external feed loss by opening connector between external and vital network
  - Only RF and RW switches are tested, RV switch is not tested
  - Test is passed when 1 switch reacts: hidden failure of switch can remain undetected
  - Test is always performed under shut-down conditions: favorable (higher) level of consumption on vital network
- Improved field test method: simulation of external feed disruption by opening connector AND trigger on low voltage
  - All types of switches are solicited; two possible configurations are tested
  - Evaluation of operation of all switches
  - Recording of system and component response
    - Frequency and tension level at switching moment
    - Time to restore nominal values
    - Power consumption

# Lay out of vital network 380V

Werking

U <352 Volt

Werking

2.250 A

Nº GEX 36.561

ALTERNATOREN 2 x 125 MVA TRANSFORMATIEPOSTEN TRANSFORTLIJNEN NAAR ANDERE CENTRALES



## Lab tests and maintenance

- Lab tests allow for individual component characterization
  - All individual components are tested (10 repetitions)
  - Effect of maintenance can be evaluated
  - Full system test after every modification
- Electro-mechanical switches are cleaned and lubricated
- Drift on settings is corrected
- Periodic maintenance scheme for components is defined

# Maintenance effect on voltage switch

	Trip Voltage before maintenance (V)										
	1	2	3	4	5	6	7	8	9	10	
ON	101,1	110,7	109,6	110,2	102,7	106,8	107,9	107,6	107,8	106,7	
OFF	113,8	113,1	112,4	112,8	114,4	109	109.3	109	109	109,4	

	Trip voltage after maintenance (V)										
	1	2	3	4	5	6	7	8	9	10	
ON	110,4	110,4	110,5	110,2	110,5	110,4	110,4	110,5	111,3	110,5	
OFF	112,1	112,3	112,4	111,9	112,4	111,9	112,1	112,4	112,4	112,3	

	Trip voltage after recalibration (V)										
	1	2	3	4	5	6	7	8	9	10	
ON	102,1	102,5	102,9	102,1	102,3	102,4	102,2	102,6	102,3	102,2	
OFF	103,1	103,3	103,6	103	103	103,4	103,4	103,1	103,1	103	

# General conclusions

#### Generic lessons learned

#### Testing for reliability of parallel systems

- Observation of functioning of individual components
- Statistics for acceptance of result: how many positive to accept one negative?
- Frequency of tests of individual components versus test to failure
- Evaluation of settings versus evolution of installation
  - Challenge to nominal thresholds with evolution in installation

#### Safety evaluation

- Passive nature of safety systems confirmed
- Diverse feed for I&C robust against malfunction of one system
- Incident management needs support from power on minimal set of instruments