

The French Energy Commission CEA  
Fuel Studies Department DEC



**IGORR 2010 Knoxville (TN-USA)  
International Group on Research Reactors**

**September 19-23, 2010**

**Replacing, refurbishing irradiated fuel rods X ray equipment**

**Francis Berdoula**

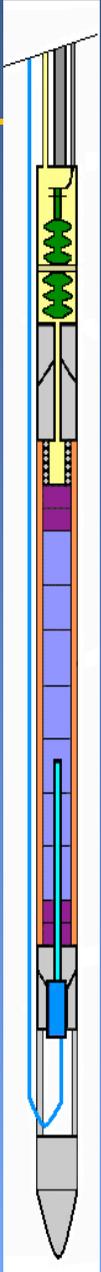
**CEA (Nuclear Energy Division) Cadarache Center  
The Fuel Studies Department DEN/DEC/SA3C/LEGEND**

**The Gas Extraction and Non-Destructive Examinations  
Laboratory in LECA Facility**



# Outline

- Objectives
- Identified Technology
- Results
- Conclusion





# Objectives

- Refurbishing X-rays equipment for fuel rod inspection
- New applications for the futur device :
  - Core inspection instrumented fuel rod
  - Enhance resolution, image contrast
  - Tomography
- Integrate the components in the actual X-rays cabine :
  - Limit civil engineering operations.



# Motivations

- Refurbishing X-ray equipment for fuel rod inspection in LECA Facility in Cadarache center :
  - 15 years of age Technology
  - Source mini-spot 160 kvolt 2 mA – mini-spot 0,2 mm
  - Image Intensifier as X-ray detector
  - Low image contrast
  - Low resolution
- New X-rays equipment :
  - High-tech components
  - Computer tomography
- Further applications :
  - Inspection in core instrumented fuel rods
  - Enhance image contrast, resolution less than 100  $\mu\text{m}$
  - Computer tomography
- Mock-up testing on standard sample
- Results
- Hot cell Implementation in 2011

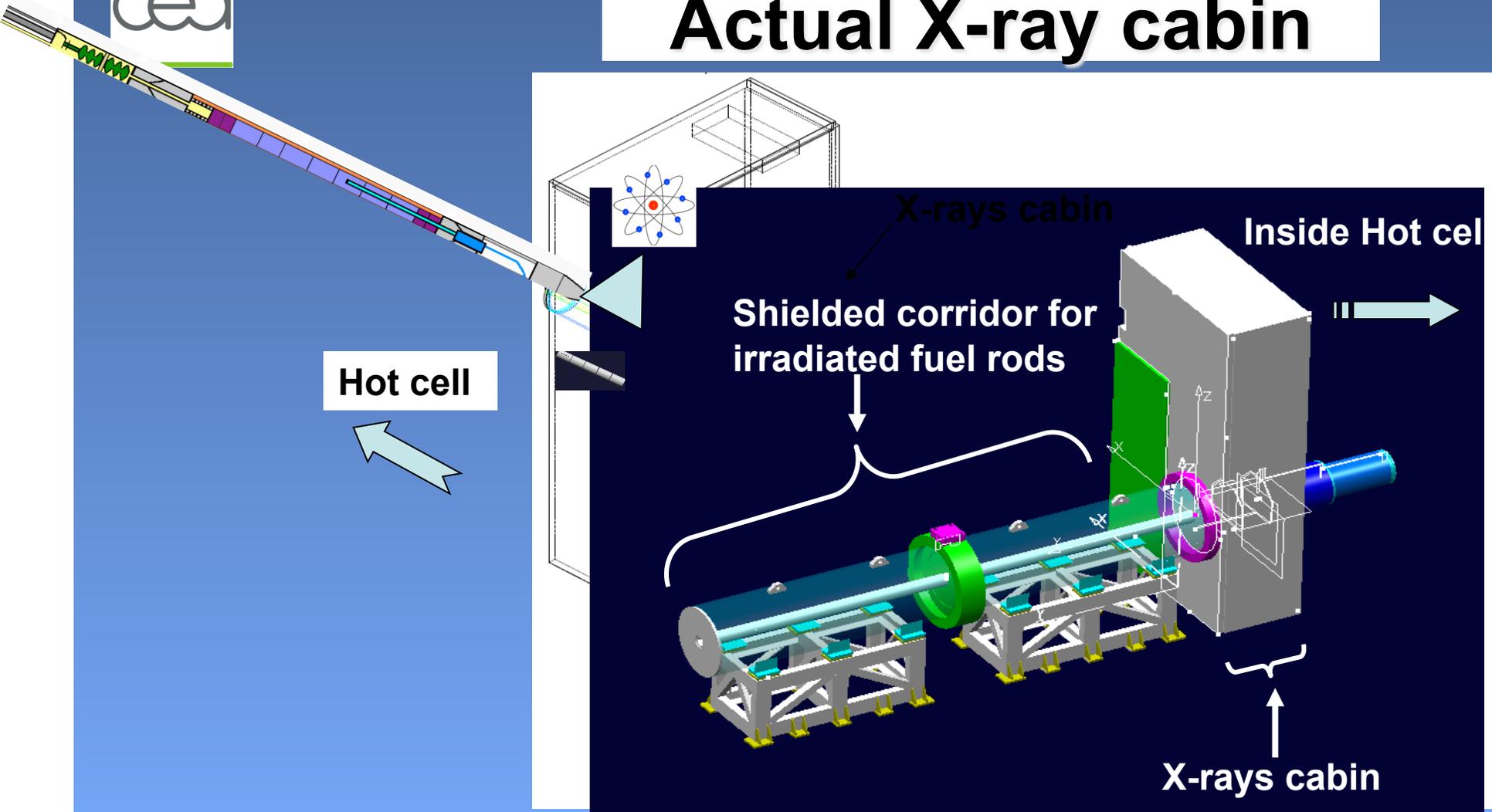


## Applications actual X rays equipment

- Fuel column length and diameter measurement
- Length and diameter pellet measurement
- Dishing
- Gap between pellets
- Gap between cladding and pellets
- End plug, spring... rod components



# Actual X-ray cabin





# Outline

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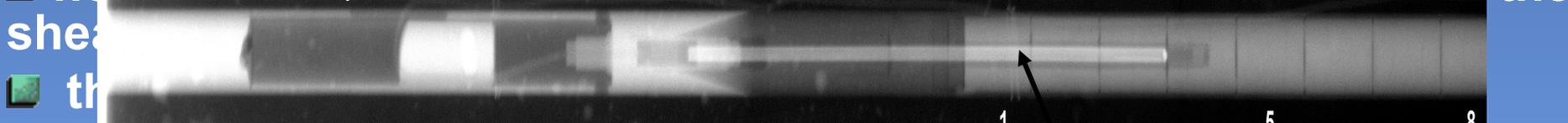
 Conclusion



# New x-rays equipment applications

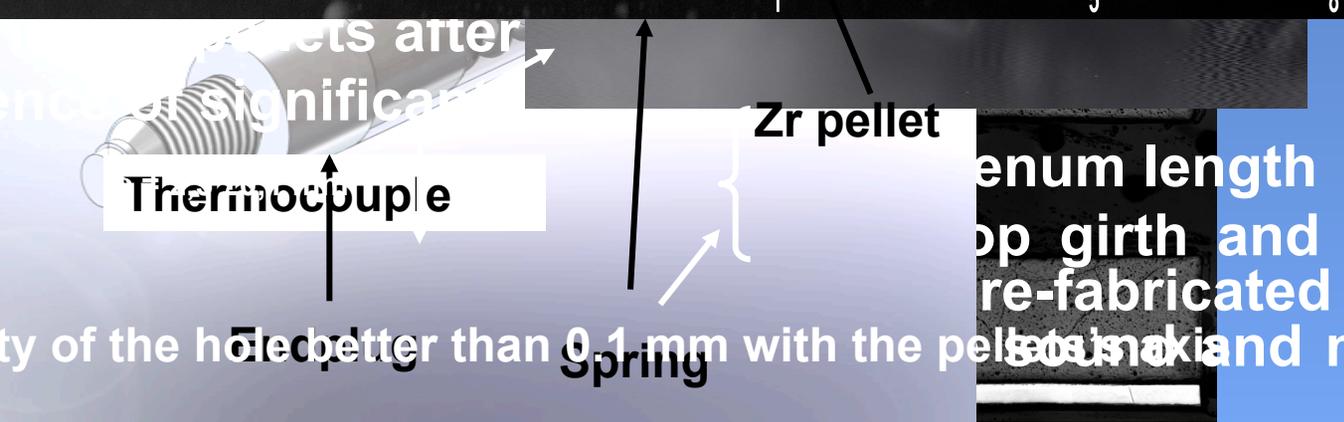
Full length x-rays will be taken of every instrumented fuel rods manufactured in LECA Facility. The

- the presence of the correct composition
- the absence of gaps in the fuel
- homogeneity of the fuel



- the flatness of the pellets after irradiation
- and the absence of significant deformation

- The x-radiography will also be used to check the length of the fuel rod, the position of the top girth and seal weld zones, the position of the re-fabricated fuel rod center with respect to the specified limit





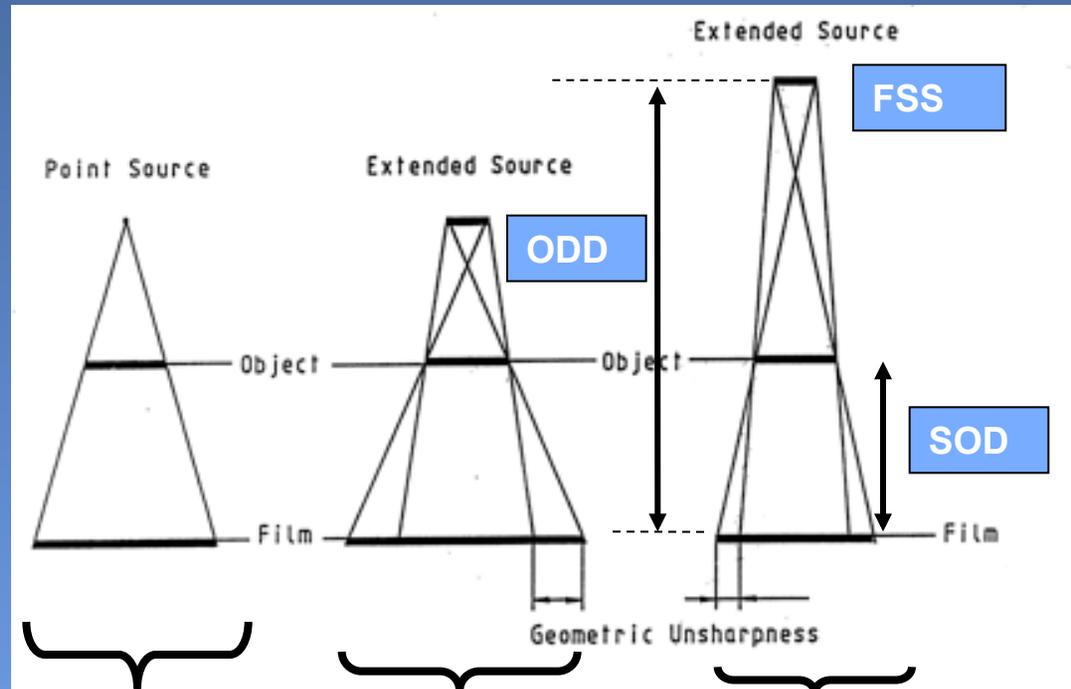
## **X ray source : Microfocus X-rays tube**

Our x-ray examinations need very high-resolution images and do therefore require x-ray tubes that can generate very small focal spot sizes. In our case, typically 100  $\mu\text{m}$  in diameter for 450 kvolt.



# Radiographic unsharpness ( $U_g$ )

## Comparison of geometric unsharpness of 3 configurations



(A) Point source

(B) Extended source

(C) Extended source  
 Further away from the Image plane

- If the focal spot is infinitesimally small, the blur is minimized because of minimal geometric bluntness
- As the focal spot increases, the blur in the image increases



## Radiographic unsharpness ( $U_g$ )

Radiographic unsharpness ( $U_g$ ) is related to the geometry of the radiographic technique and simply put, is the amount of 'blur' present in a radiography image.

The primary factors contributing to  $U_g$  in the radiographic technique are:

1. A large focal spot :  
(point from which the usable radiation beam emanates). In X-ray tubes, this is the area where high speed electrons are focused onto the target, resulting in the generation of photons.
1. Excessive object to detector distance, as related to focal spot size (FSS).

$U_g$  for any radiographic technique can be easily calculated using the following formula:

$$U_g = \frac{FSS \times ODD}{SOD}$$

**FSS = Focal spot size**

**ODD = Object to detector distance**

**SOD = Source to object distance**

For our X-ray cabin,  $U_g$  will be minimized by using a micro spot, keeping the fuel rod as close to the digital detector as possible. In our case this distance is limited by biologic protection around the specimen.

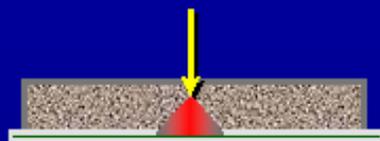


## X-ray scintillator conversion: ( $Gd_2O_2S$ , CsI compounds)

### Unstructured (turbid) phosphor

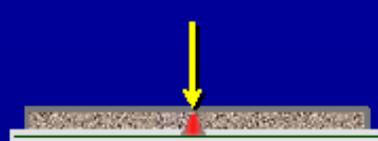
#### Thick Screen:

- Good Absorption
- Poor Resolution



#### Thin Screen:

- Poor Absorption
- Good Resolution



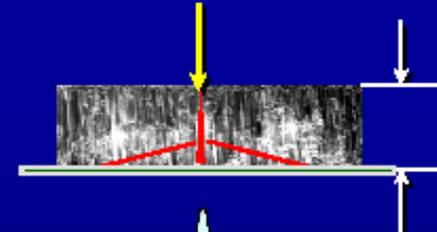
LSF

Resolution limit

### Structured phosphor

#### Thick Screen:

- Good Absorption
- Good Resolution



Light Pipe  
(Optical Fiber)

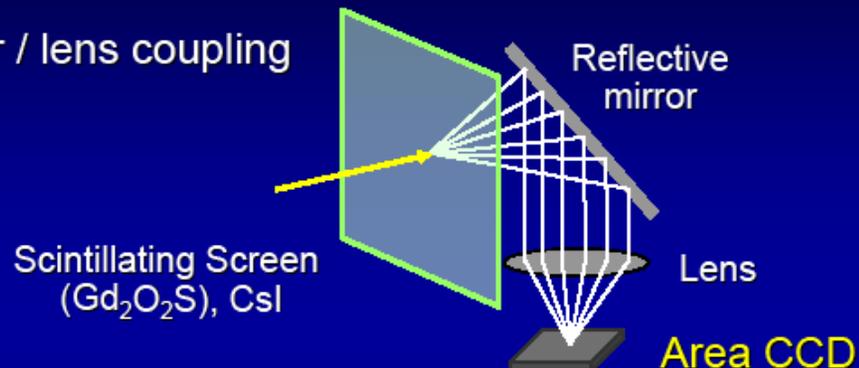




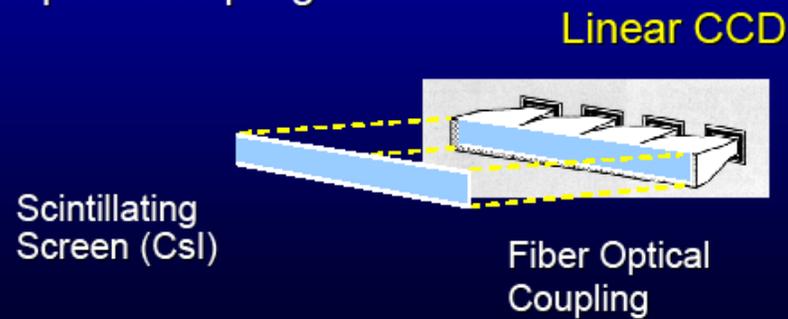
“Indirect” x-Indirect detector: a conversion of x rays into light by a scintillator, *and* light into electrons for signal capture

## CCD-based DR systems

- Area Scintillator / lens coupling



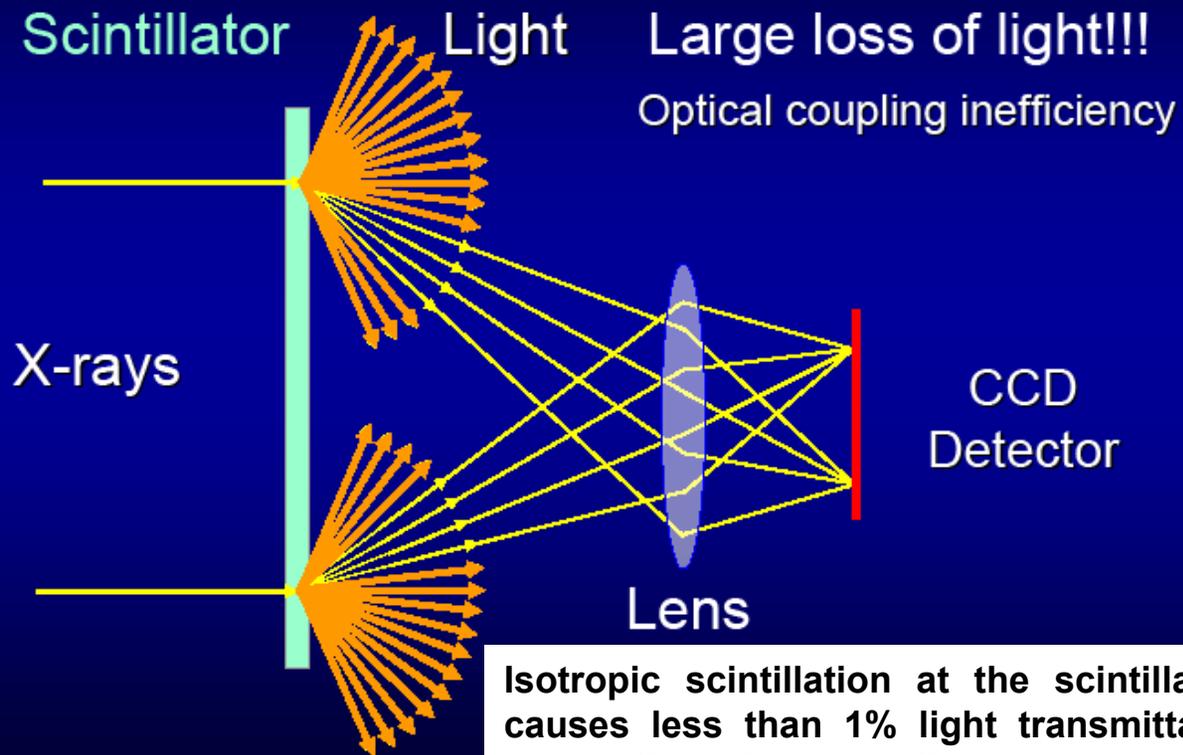
- Slot scintillator / fiberoptical coupling





**Schematic illustration of the lens coupling between a scintillator and a CCD detector.**

**Light emission & Optical coupling**



**Isotropic scintillation at the scintillator surface causes less than 1% light transmittance with a conventional lens coupling.**



# Collection efficiency for lenses

## Collection efficiency for lenses

$$\eta_L = \frac{T_L}{1 + 4 \cdot f_{\#}^2 \cdot (1 + m)^2}$$

- Assuming Lambertian source of light

$T_L$  = transmission factor of lens

$f_{\#}$  = f-number of lens

$m$  = demagnification factor

- Note  $f_{\#}$  and  $m$  appear as squared terms

### Example

$$f_{\#} = 1.2, \quad T_L = 0.8, \quad \text{and} \quad m = 2$$

$$\eta_L = 1.5\%$$



## Collection efficiency – fiber optic

$$\eta_{TFO} = \left(\frac{1}{m}\right)^2 \cdot \left(\frac{(n_2^2 - n_3^2)^{1/2}}{n_1}\right)^2 \cdot T_F \cdot (1 - L_R) \cdot F_C$$

Asuming Lambertian source as before

m = demagnification factor

$n_1, n_2, n_3$  = refraction indices of sources medium, fiber core and cladding

$T_F$  = loss due to Fresnel reflection

$F_c$  = fill factor of core

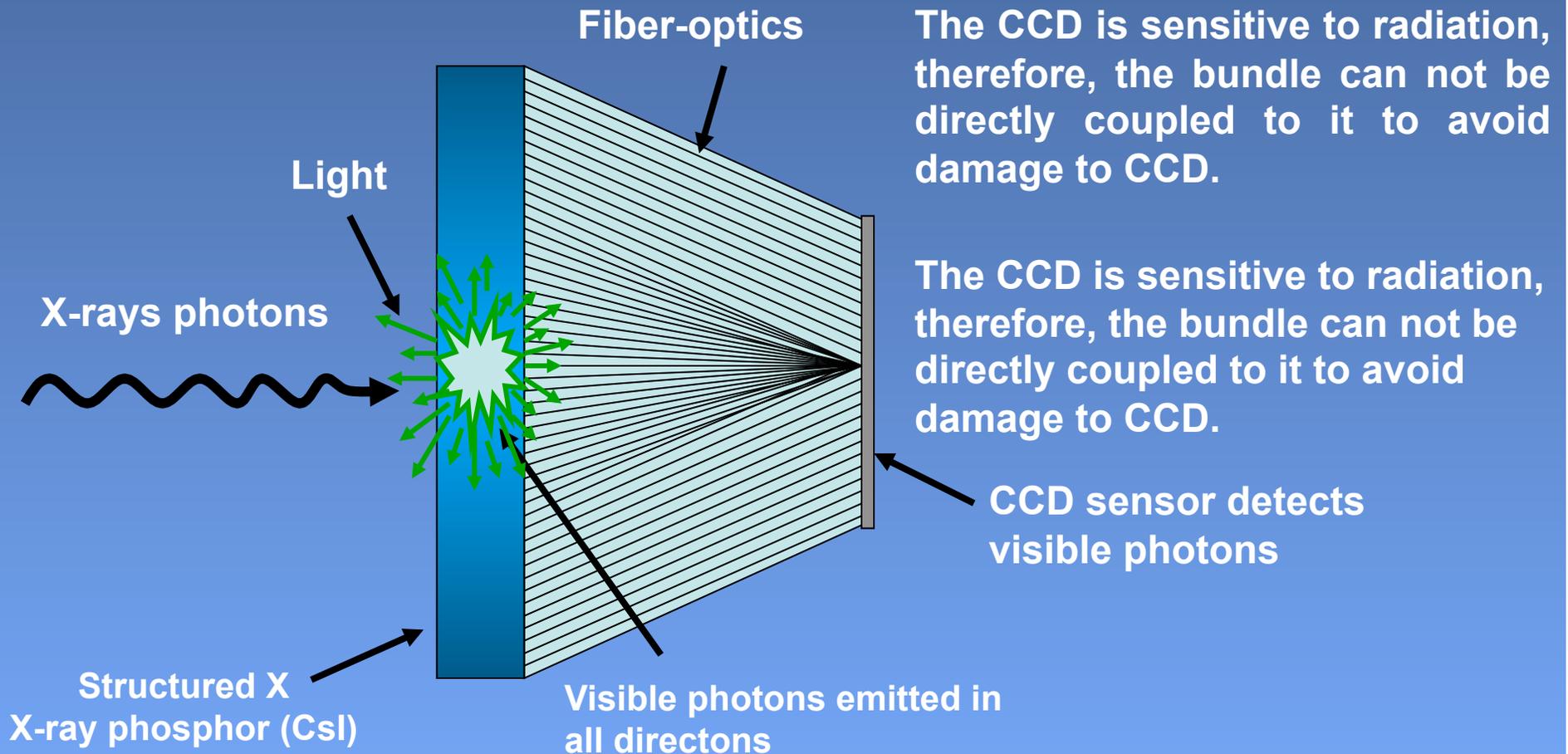
Examples : m = 2;  $n_1 = 1$ ;  $n_2 = 1,8$ ;  $n_3 = 1,5$ ;  $T_F = 0,8$

$F_c = 0,85$  and  $L_R = 0$

$\eta = 15\%$

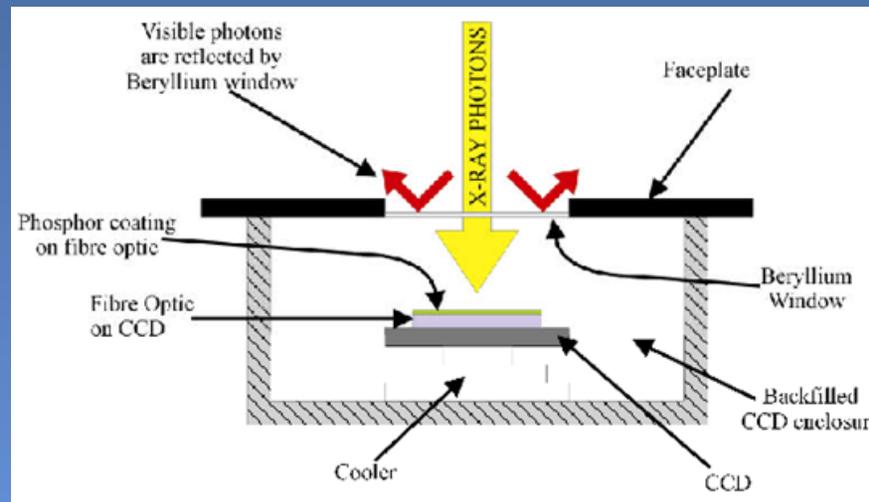


# Indirect detection principle





# Indirect X-rays sensor

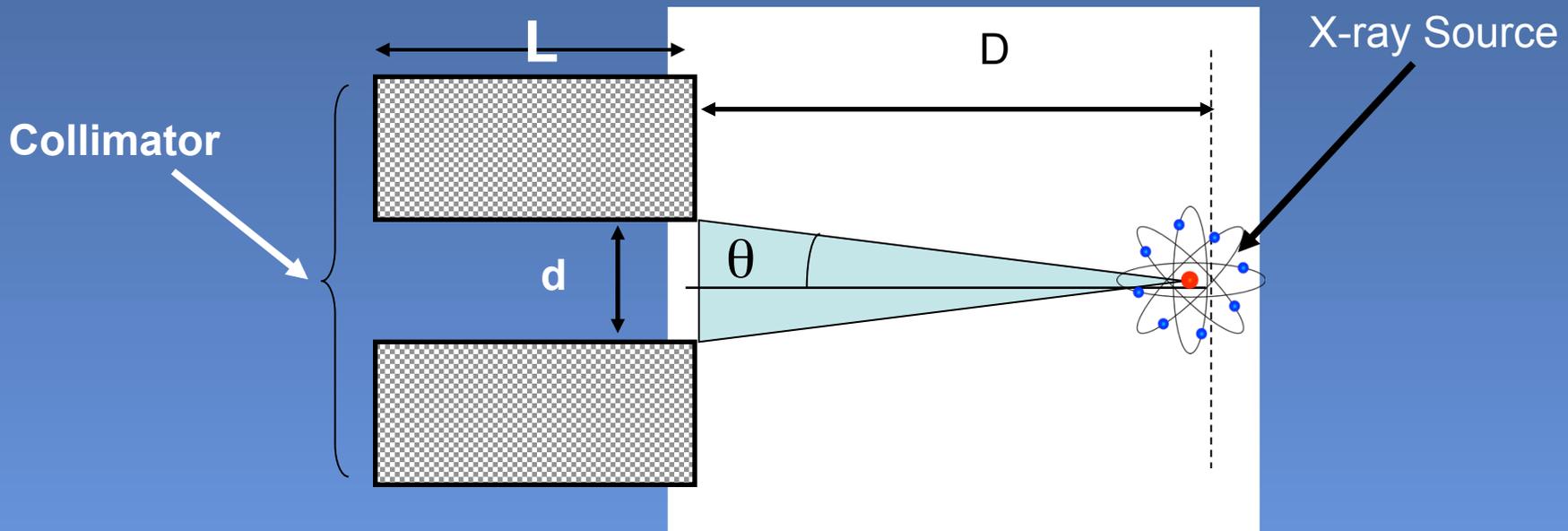


Indirect detection is used for hard X-ray detection and when you need:

- Single photon sensitivity even with highly demagnifying
- tapers (EMCCD technology available)
- QE (Quantum Efficiency) coverage that stretches well into the hard x-ray region
- Large area coverage (via magnifying taper)
- High dynamic range at high energy levels
- Protection of the CCD sensor



# X Rays source general characterizations



D distance from collimator, d diameter slot, L collimator length

■ Resolution proportional to  $\theta$

■ Resolution proportional to Distance from Source



## Spatial Resolution

- R is an indicator of spatial resolution
- Spatial resolution degrades rapidly with increasing collimator-to-object distance  $D$
- Size of the image produced by parallel-hole collimator not affected by distance of object from collimator



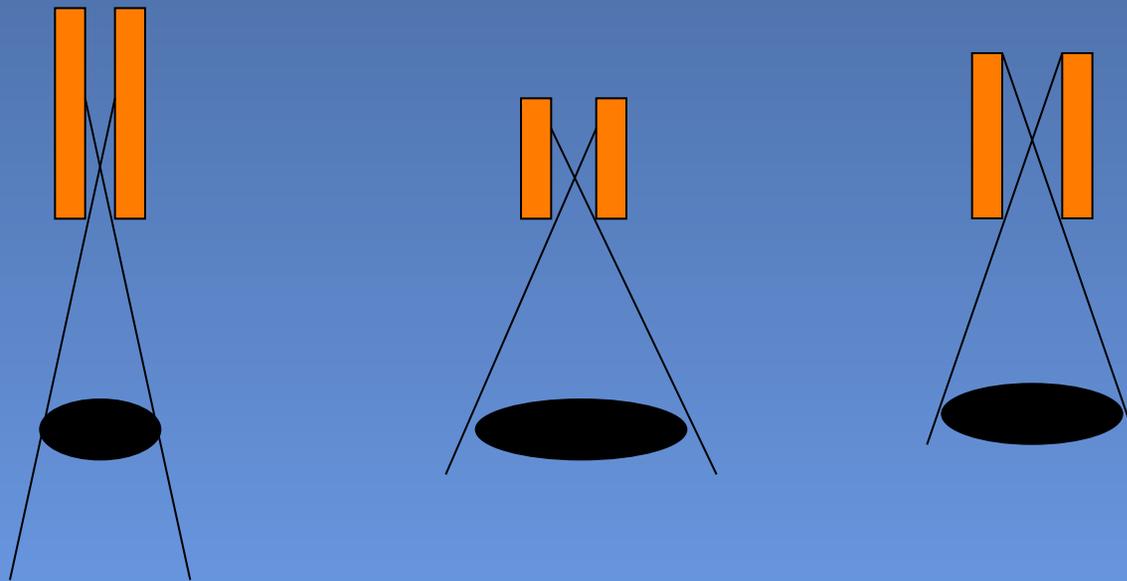
# Spatial Resolution

Geometrical resolution  $R_g \sim \frac{d \times (L + D)}{L}$

- As  $d$  increases,  $R_g$  increases (resolution is worse)
- As  $L$  increases,  $R_g$  decreases (resolution is better)
- As  $D$  increases,  $R_g$  increases (resolution is worse)



# Sensitivity



From geometrical considerations, sensitivity is dependent on area seen by hole

$$\text{Sensitivity} \sim (Rg)^2$$



# Sensitivity

- Sensitivity = efficiency of the collimator
- Sensitivity = the ratio of the number of photons that pass through the collimator to the number emitted
- Resolution is better as  $R_g$  decreases but sensitivity is much worse as  $R_g$  decreases (influence is squared)
- Thus efforts to improve resolution and sensitivity go in opposite directions
- So choice of collimator is a tradeoff between spatial resolution and sensitivity



# Outline

 Objectives

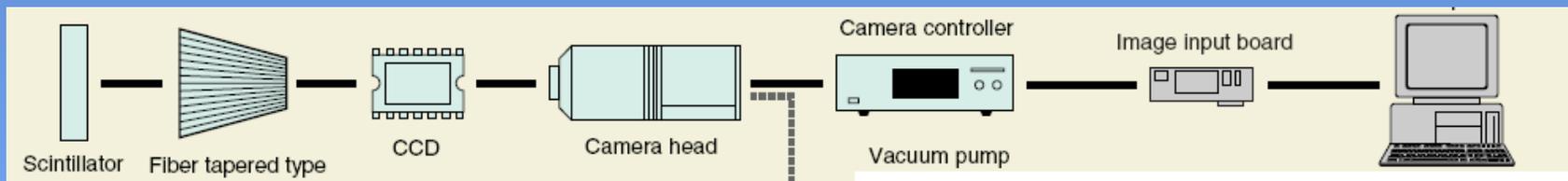
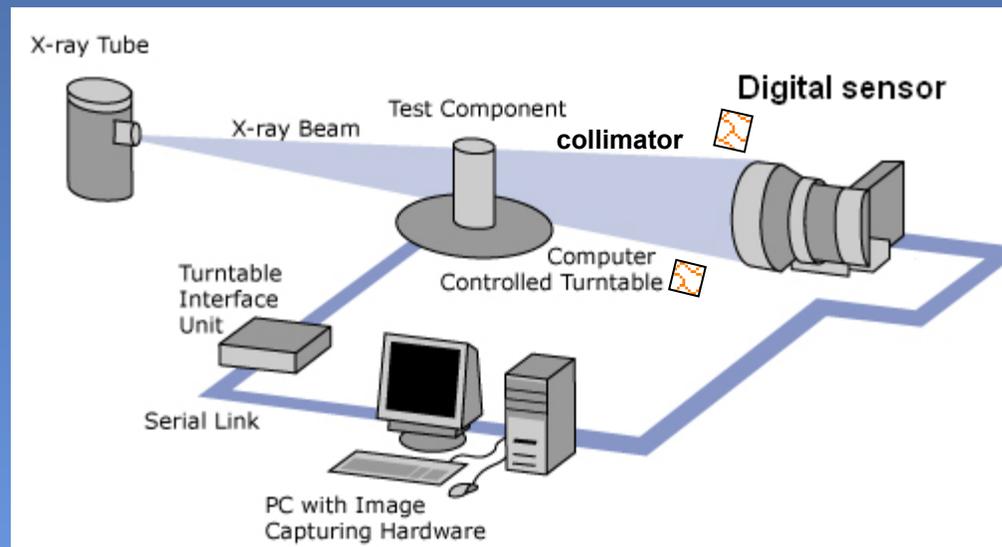
 Identified Technology

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# X-ray equipment



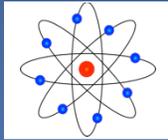
**Digital X-ray detector : scintillator coupled with ccd sensor by fiber optics**



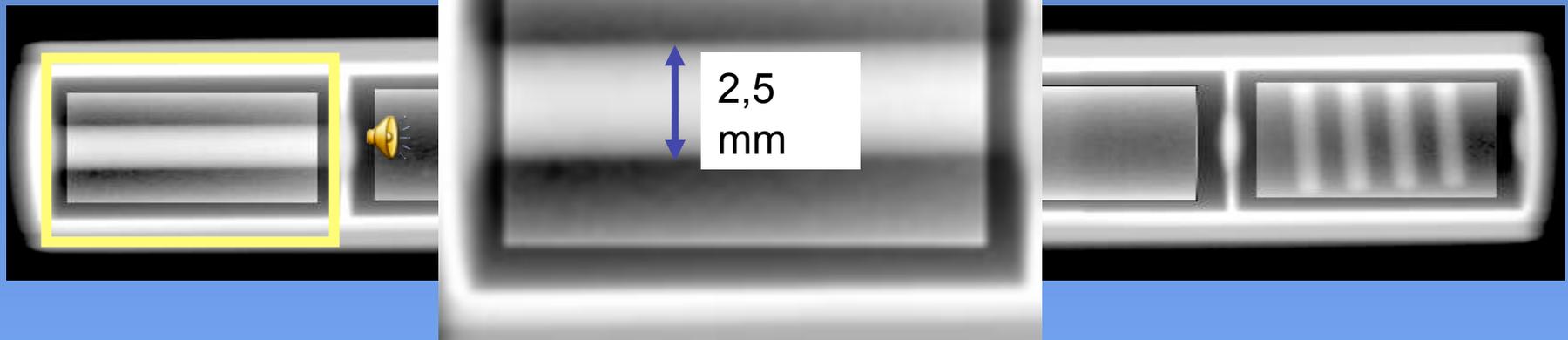
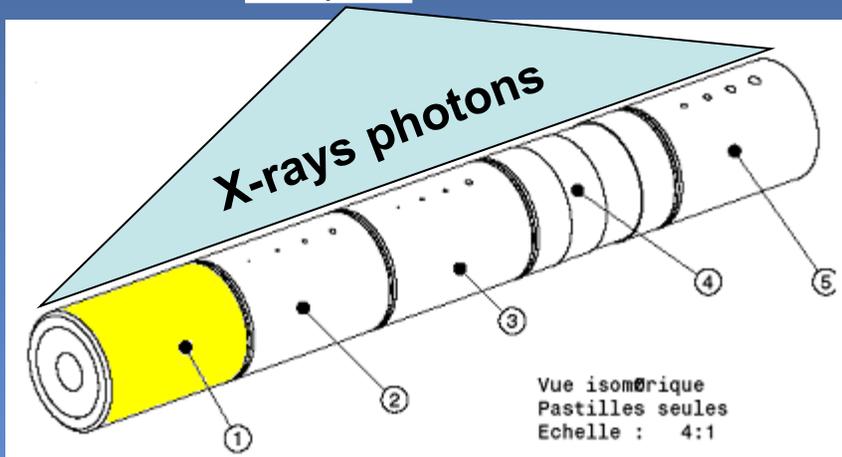
## Main Test Parameters

- X-ray high voltage 450kV
- X-ray tube current 1.55mA
- Geometrical magnification 2.7
- Focal spot size 0.1 mm
- 100  $\mu\text{m}$  slot lead collimator
- Indirect sensor 25  $\mu\text{m}$  pixel size
- Integration time 1 - 64 seconds

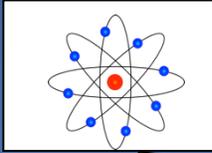




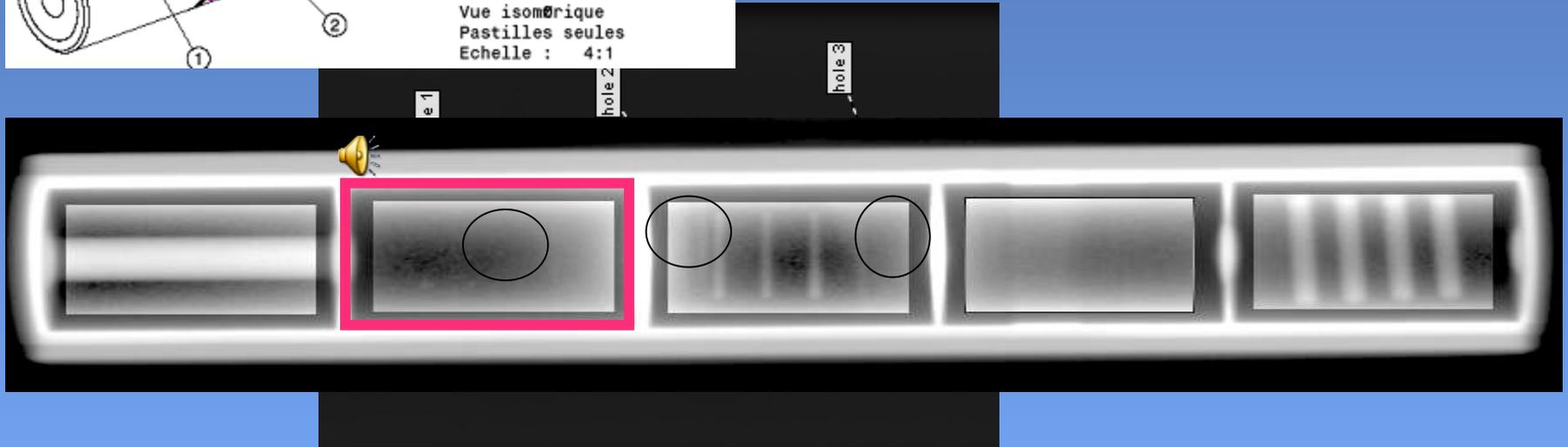
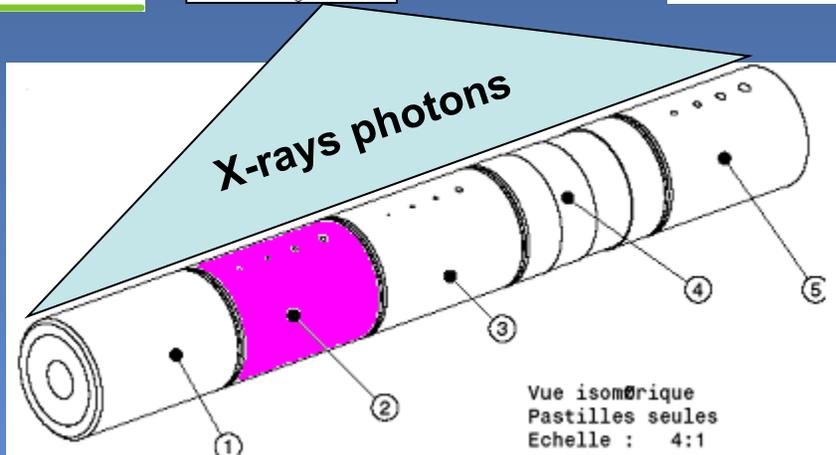
# Pellet 1 digital radiography



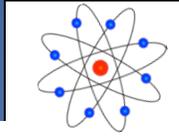
Orientation 0°, 450kV, 1.55mA, 64s integration time, original x-ray image without digital filtering.



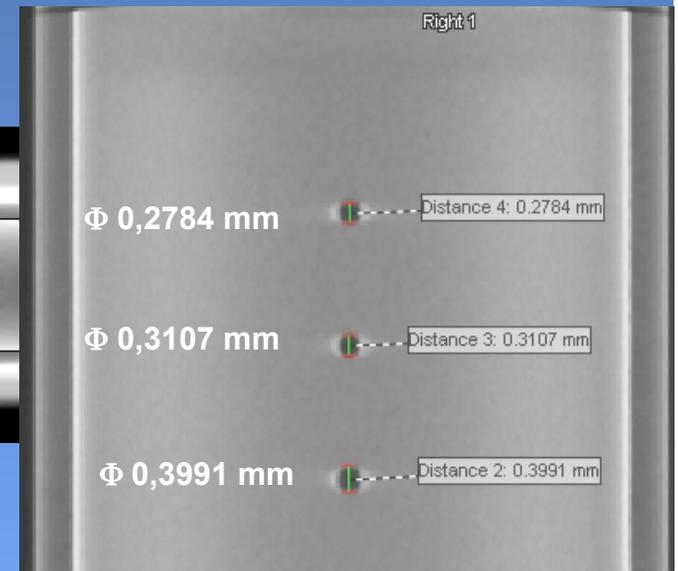
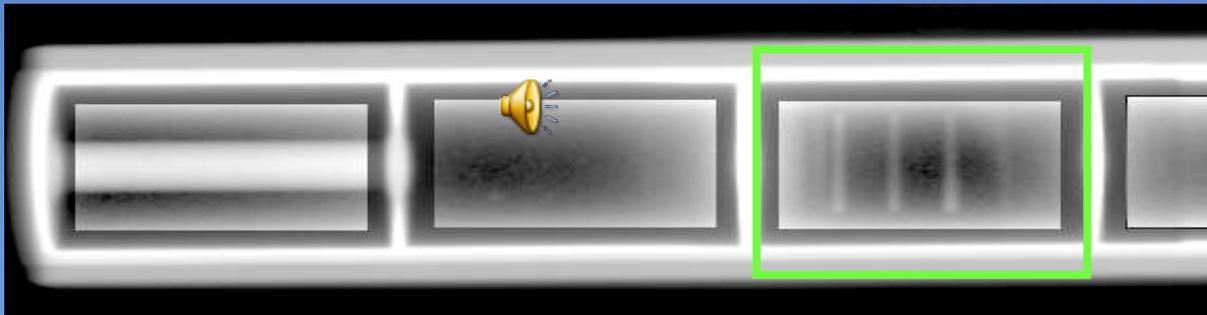
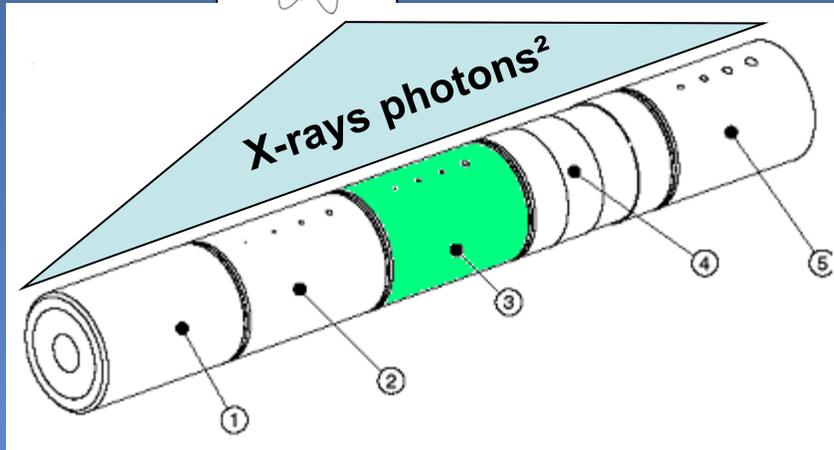
# Pellet 2 digital radiography



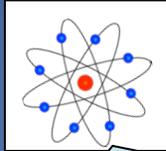
Orientation 0°, 450kV, 1.55mA, 64s integration time, original x-ray image without digital filtering.



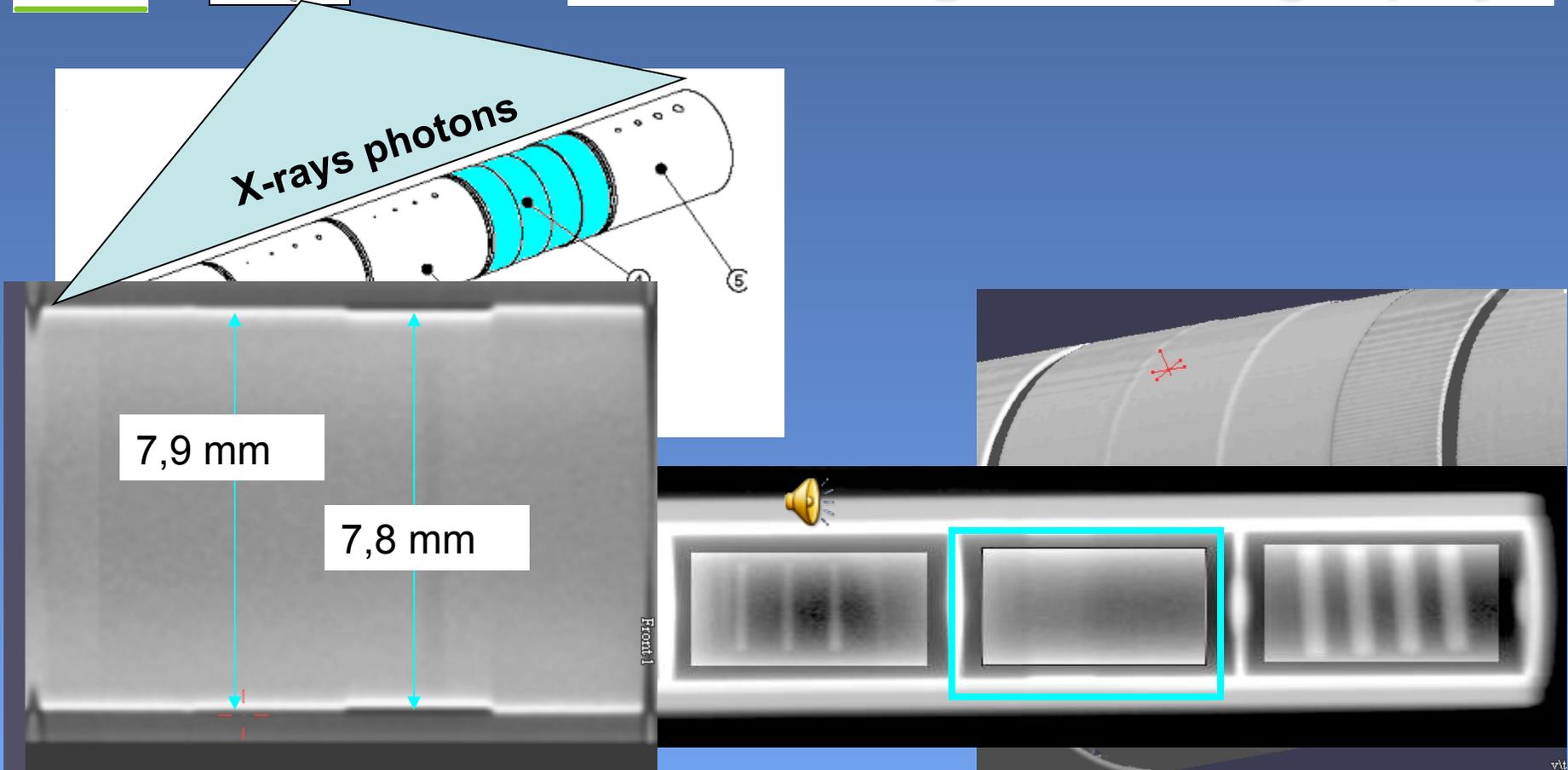
# Pellet 3 digital radiography



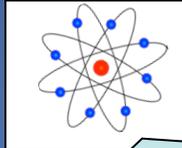
Orientation 0°, 450kV, 1.55mA, 64s integration time, original x-ray image without digital filtering.



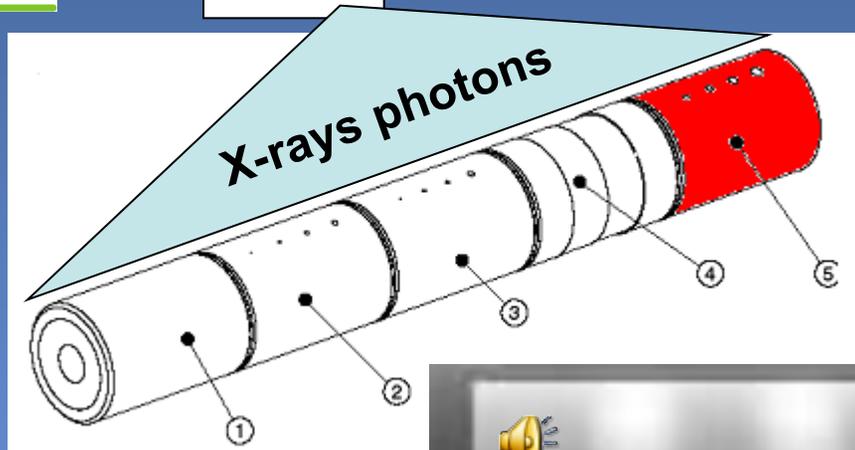
# Pellet 4 digital radiography



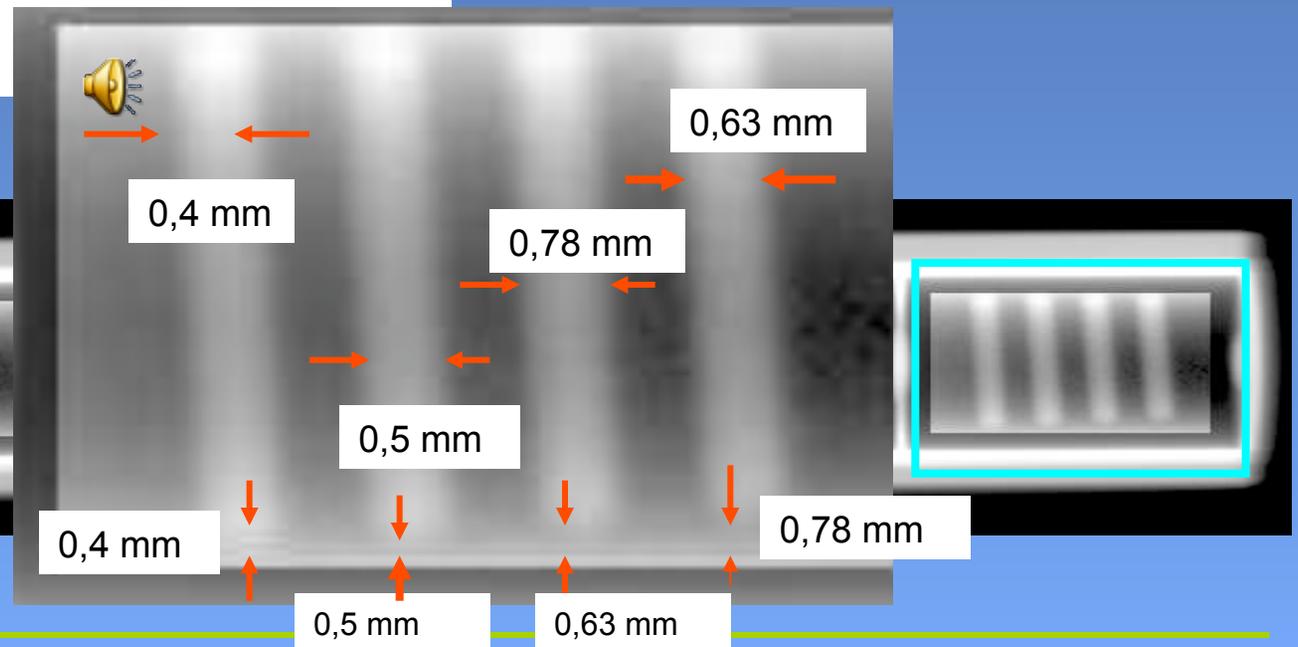
Orientation 0°, 450kV, 1.55mA, 64s integration time, original x-ray image without digital filtering.



# Pellet 5 digital radiography



Orientation 0°, 450kV,  
1.55mA, 64s  
integration time,  
original x-ray image  
without digital filtering.





# Outline

■ Objectives

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## Conclusion

- X rays tests in a mock-up
- Identification suitable X-rays cabin components
- Simulation confirms our components and predict the future device performance. One of the strong points of this tool is to integrate gamma background
- Actual X-rays cabin is dismantling
- New X-ray equipment implementation is planned for 2011
- This X ray equipment will be a complement to fast neutron radiography



**Thank You for Your  
Attention !**

**Any questions ?**